#### **Third Virial Coefficients**

#### **Silicon Valley FIG**

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#### Summary

Gas-Liquid-Solid Equilibrium 2<sup>nd</sup> and 3<sup>rd</sup> Virial coefficient Van der Waals, 1873 Virial Equation of state, 1906 Beattie–Bridgeman, 1928 Benedict-Webb-Rubin, 1940 Starling-Hans, 1972 Lee-Kesler, 1975 Cubic Virial Equation, 2017

#### **Original Paper in 1972**

#### THE GAS-LIQUID-SOLID EQUILIBRIUM STUDIED BY A SIMPLE EQUATION OF STATE

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#### Abstract

The van der Waals' equation of state is modified by adding a correction term to become:

 $P = RT/(V-b) - a/V^2 - e/((V-c)^2 + d^2)$ 

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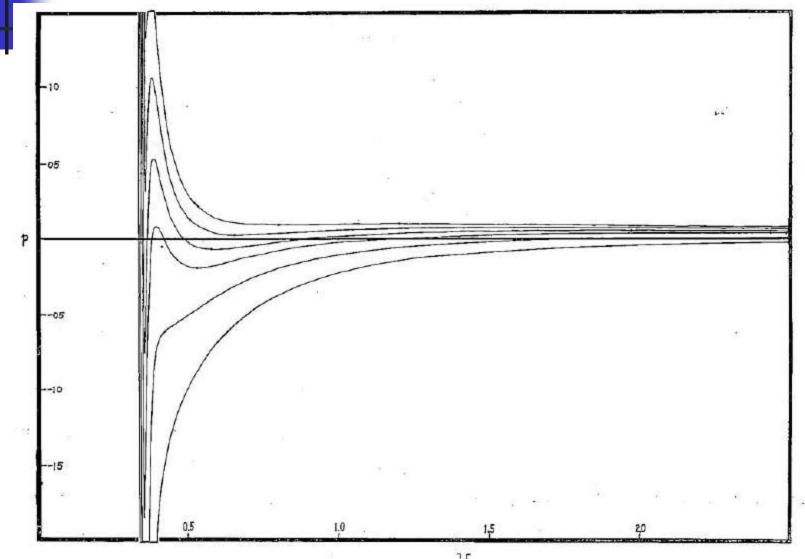
This equation is capable of describing all the essential features of the equilibrium among the gaseous, liquid and solid phases of a pure compound. Preliminary results are given for carbon dioxide. Quantitative treatments are currently in progress.

#### **A Desktop Wang Computer**



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#### **Plot on Wang Computer**



#### **Gas-Liquid-Solid Phases**

The best virial EOS is with n=26:  $p = 3t/v - 3(1 - v_s/v)(1 - (v_m/v)^{26})(1 - (v_l/v)^{26})/v^2$ For Argon at the triple point, t=0.553 p=0.0142 v<sub>c</sub>=0.330 v<sub>1</sub>=0.378 v<sub>m</sub>=0.354 n=26



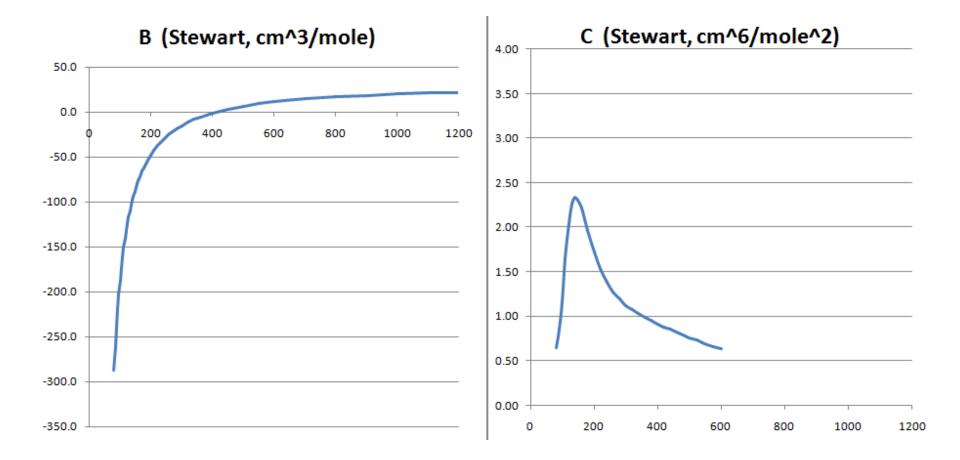
## 2<sup>nd</sup> and 3<sup>rd</sup> Virial Coefficients

The 2<sup>nd</sup> and 3<sup>RD</sup> virial coefficients had been studied for more than 100 years.

All existing studies showed that they are not correlated.

Argon has been a typical gas for extensive experimental studies.

## 2<sup>nd</sup> and 3<sup>rd</sup> Virial coefficients of Argon



#### **Virial Equation of State**

Compressibility Z as a function of density ρ and temperature T: Z=P/RTρ= (1+Bρ+Cρ<sup>2</sup>+Dρ<sup>3</sup>+Eρ<sup>4</sup>+Fρ<sup>5</sup>+Gρ<sup>6</sup>+...)

Virial coefficients B-G... depend only on temperature.

## Van der Waals, 1873

#### $P=RT/(v-b) + a/v^2$

#### It can be recast in virial form:

#### $Z=1+(b-a/RT)/v+b^2/v^2+b^3/v^3+b^4/v^4+...$

Third virial coefficient is a constant b<sup>2</sup>.

#### Beattie–Bridgeman, 1928

$$P=RT (1-c/vT^{3})(v+B) / v^{2}-A/v^{2}$$
$$A=A_{0}(1-a/v)$$
$$B=B_{0}(1-b/v)$$

# $Z=1+(B_0-A_0/RT-c/T^3)/v$ $-(B_0b-A_0a/RT+B_0c/T^3)/v^2+B_0bc/T^3v^3$ The third virial coefficient is negative.

#### **Benedict-Webb-Rubin, 1940**

 $P = RT\rho + (B_{0}RT - A_{0} - C_{0}/T^{2})\rho + (bRT - a/T)\rho^{2}$  $+aa\rho^{5}+(c/T^{2})(1+v\rho^{2})(exp(-v\rho^{2}))\rho^{3}$ 

#### $Z=1+(B_0-A_0/RT-CO/RT^3)\rho$ +(b-a/RT) $\rho^{2}$

 $+(a\alpha/RT)\rho^{5}+(c/RT^{3})(1+\gamma\rho^{2})(exp(-\gamma\rho^{2}))\rho^{3}$ 

The exponential term is troublesome.

#### **Benedict-Webb-Rubin, 1940**

The exponential term is rapidly converging, and can be expanded:  $exp(-\gamma\rho^2)=1-\gamma\rho^2$ 

Then, it has a much simpler virial form:  $Z=1+(B_0-A_0/RT-CO/RT^3)\rho$   $+(b-a/RT+c/RT^3)\rho^2$  $+(a\alpha/RT)\rho^5-(c/RT^3)\gamma^2\rho^6$ 

#### Starling-Hans, 1972

## $P=RT\rho+(B_0RT-A_0-C_0/T^2+D_0/T^3-E_0/T^4)\rho +(bRT-a+d/T)\rho^2 +a(a+d/T)\rho^5+(c/T^2)(1+\gamma\rho^2)(exp(-\gamma\rho^2))\rho^3$

Then, it has a virial form:  $Z=1+(B_0-A_0/RT-C_0/RT^3+D_0/RT^4-E_0/RT^5)\rho$   $+(b-a/RT-d/RT^2+ c/RT^3)\rho^2+$  $\alpha(a/RT+d/RT^2)\rho^5+(c/RT^3)\gamma^2\rho^6$ 

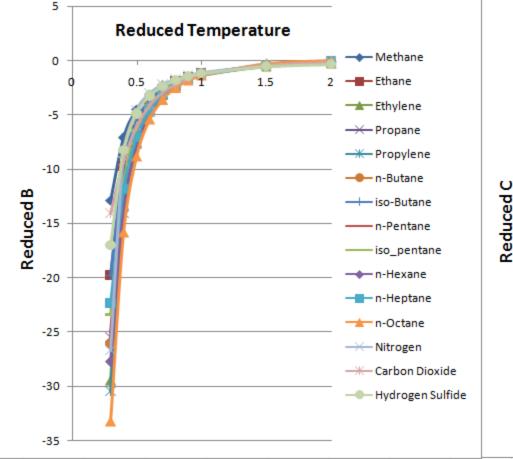
#### Lee-Kesler, 1975

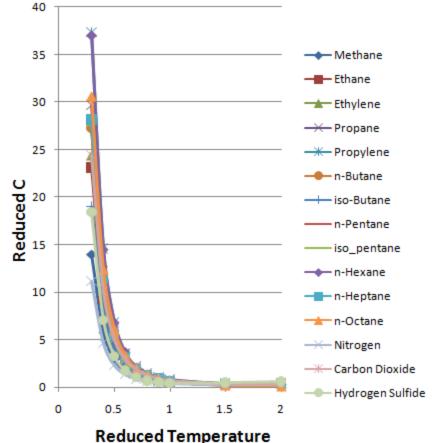
## A single equation generalized for many different compounds:

## $$\begin{split} Z = 1 + (b_1 - b_2/t - b_3/t^2 - b_4/t^3)\rho \\ + (c_1 - c_2/t + c_3/t^3)\rho^2 \\ + (d_1 + d_2/t)\rho^5 + (c_4/t^3)(\beta + \gamma\rho^2)(exp(-\gamma\rho^2))\rho^3 \end{split}$$

#### $t=T/T_c$ and $\rho=RT_c/P_cV$

#### Starling-Hans, 1972





#### A virial EOS truncated to the third term $P = (RT/v)(1+B/v+C/v^2)$

It has all the nice properties of van der Waals EOS, but without the singular point.



At the critical point, assuming: dP/dv=0; and d<sup>2</sup>P/dv<sup>2</sup>=0

Cubic virial equation can be solved to get:  $B=-v_c$ ;  $C=v_c/3$  and  $Z_c=0.333$ 

 $Z_c$  is better than what van der Waals results, 0.375, but still not close to actual values , 0.26-0.30.



Cubic virial equation dominates the virial equation of state, and should be studied more carefully and more thoroughly.

The second and third virial coefficients in the reduced forms still show divergent behavior, and need more studies.



Virial equations were generally constructed with 'multiproperty analysis' or 'multivariable regression', and you don't know what happened underneath.

Now, cubic virial equation can be constructed first using 'second order regression' to obtain 2<sup>nd</sup> and 3<sup>rd</sup> coefficients. Residues can be analyzed separately.



Using cubic virial equation, 2<sup>nd</sup> and 3<sup>rd</sup> coefficients can be solved analytically in the saturation region. They should be used to check results from second order regressing.

Residues from higher virial coefficients must be analyzed after 2<sup>nd</sup> and 3<sup>rd</sup> coefficients are determined precisely.



#### Conclusions

Properly determined 3<sup>rd</sup> virial coefficients will reduce complexity in virial EOS, and improve its accuracy.

My cubic virial EOS has great value in improving our understanding of real gases, particularly in the saturation region.





#### **Thank You Very Much!**

